

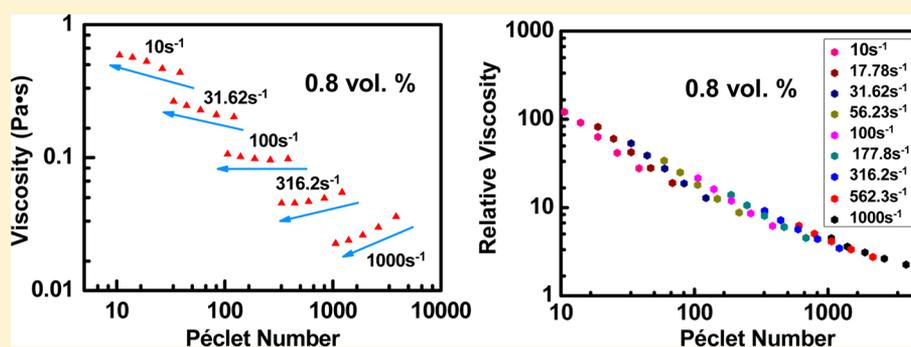
Viscosity and Thermal Conductivity of Stable Graphite Suspensions Near Percolation

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ABSTRACT: Nanofluids have received much attention in part due to the range of properties possible with different combinations of nanoparticles and base fluids. In this work, we measure the viscosity of suspensions of graphite particles in ethylene glycol as a function of the volume fraction, shear rate, and temperature below and above the percolation threshold. We also measure and contrast the trends observed in the viscosity with increasing volume fraction to the thermal conductivity behavior of the same suspensions: above the percolation threshold, the slope that describes the rate of thermal conductivity enhancement with concentration reduces compared to below the percolation threshold, whereas that of the viscosity enhancement increases. While the thermal conductivity enhancement is independent of temperature, the viscosity changes show a strong dependence on temperature and exhibit different trends with respect to the temperature at different shear rates above the percolation threshold. Interpretation of the experimental observations is provided within the framework of Stokesian dynamics simulations of the suspension microstructure and suggests that although diffusive contributions are not important for the observed thermal conductivity enhancement, they are important for understanding the variations in the viscosity with changes of temperature and shear rate above the percolation threshold. The experimental results can be collapsed to a single master curve through calculation of a single dimensionless parameter (a Péclet number based on the rotary diffusivity of the graphite particles).

KEYWORDS: Percolation, viscosity, shear thinning, graphite suspensions

Colloidal solutions with well-dispersed nanoparticles, also called nanofluids,¹ have attracted extensive attention due to their abnormal thermal conductivity enhancement and the potential applications in energy technologies.^{2–8} Heat conduction in nanofluids has been extensively studied,^{9–16} and the variation in results has led to much debate as to the mechanisms of thermal conduction in nanofluids. By freezing nanofluids consisting of alumina nanoparticles in different base fluids, Gao et al.¹⁶ demonstrated that clustering is a key factor for enhancing the thermal conductivity. Zheng et al.¹⁷ observed peculiar percolation phenomena in the thermal conductivity for stable graphite suspensions. Below the percolation threshold, the thermal conductivity increases faster with increasing graphite loading than above the percolation threshold, which is directly in contrast with the electrical conductivity results.

Combined with AC impedance spectroscopy studies, they interpreted this observation that there is an abrupt reduction in the slope of the thermal conductivity enhancement after percolation as most likely related to the role of the interfacial energy of the particle clusters before and after percolation. These studies established that Brownian motion and diffusive contributions of graphite flakes were not responsible for the experimentally observed thermal conductivity enhancement.

The rheology of nanofluids and suspensions is another important material property for practical applications,^{18–25} especially for flow-based application such as all kinds of

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coolants in pipe cooling systems. For simple Newtonian fluids (water, ethylene glycol, etc.), the shear viscosity is solely a function of temperature and is independent of the shear rate. However, for non-Newtonian fluids such as polymer melts, blood, and ketchup, the shear viscosity is not only a function of temperature but also a function of the shear rate and shear history.^{26–31} Past work has shown that the steady shear viscosity $\eta(\dot{\gamma}, T)$ of nanofluids typically decreases with increasing temperature at a fixed shear rate.^{32–37} Although the viscosity of suspensions has been extensively studied in the literature,^{21,37–42} there have been few studies that focus on thermal effects on the macroscopic suspension viscosity when the volume loadings pass from the dilute regime into the percolated regime. In this work, we measure the thermal conductivity and viscosity of graphite suspensions as a function of temperature and volume fraction, focusing on the percolation behavior. We observe two distinct trends for thermal conductivity and viscosity below and above percolation. From our analysis of the experimental data, we conclude that a diffusive Brownian contribution of the dispersed colloidal structures remains important in the measured viscosity above the percolation threshold despite its insignificance for the thermal conductivity.

Graphite flakes are first prepared by sulfuric acid intercalation, which exfoliates the natural graphite into graphite flakes and then expands via microwave radiation.^{17,43–45} The expanded graphite flakes are then mixed with ethylene glycol. The suspensions are ultrasonicated for 35 min to disperse the particles and to form stable graphite dispersions. Samples of different volume fraction are prepared by diluting the concentrated 1 vol % suspension ensuring the graphite flakes are from the same fabrication batch for all samples. The SEM image in Figure 1a reveals the typical morphology of the graphite flakes. The individual graphite particles have diameters of several micrometers but, as can be observed from the optical microscope image shown in Figure 1b, the flakes form much larger clusters. The clusters are isolated from each other when the graphite volume fraction is low (typically less than $\phi < 0.07$ vol %) and merge to form a percolation network when the graphite volume fraction is high (typically higher than $\phi \geq 0.1$ vol %).^{17,46} Our previous studies based on electrical conductivity, AC impedance spectroscopy, and thermal conductivity measurements have established that such nanofluids have a percolation threshold around $\phi_c \approx 0.07\%$ volume fraction for an ethylene glycol based dispersion.

The viscosity of the graphite dispersion at room temperature is measured using a controlled stress rheometer (TA Instruments AR-G2) with a cone-and-plate geometry. The viscosity results show good repeatability; during repeated measurements with the same suspension the viscosity curves coincide with each other with standard deviation less than 2%. Two key trends of viscosity with shear rate are evident in Figure 2. First, the viscosity of the graphite suspension increases as the volume fraction increases. Second, the graphite suspension exhibits non-Newtonian behavior. Specifically, the viscosity decreases with increasing shear rate (i.e., the dispersion is shear thinning), and the level of shear thinning increases for higher volume fractions. This is likely due to the graphite clusters and flakes preferentially realigning themselves along the flow direction under the application of an imposed shear stress. This structural reorganization reduces particle–particle interactions and thus reduces the viscosity.

In a previous paper,¹⁷ some of the present authors observed that the thermal conductivity of graphite suspensions increases

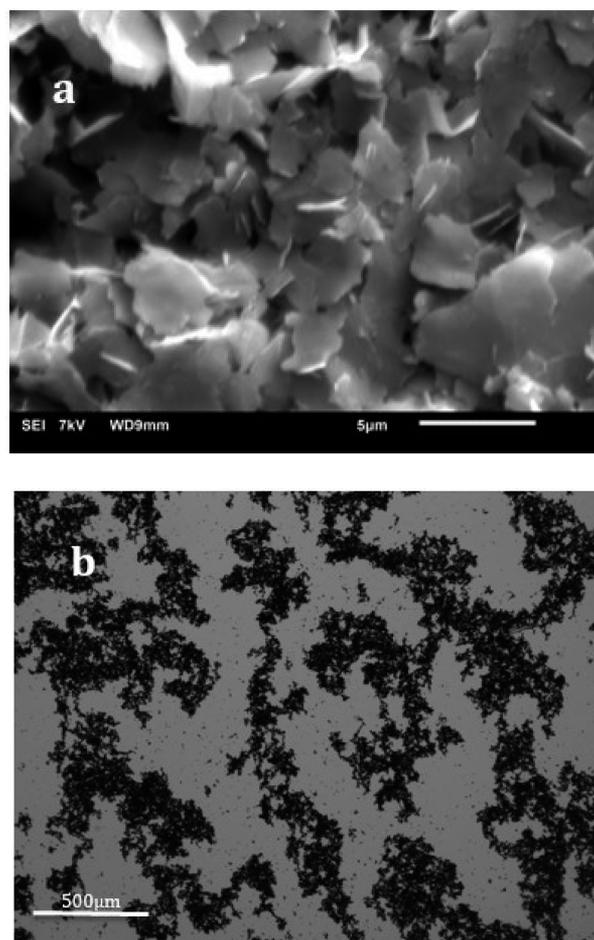


Figure 1. Microstructure of graphite flakes. (a) SEM image of individual graphite flakes in the dry state. (b) Optical image of a graphite suspension above the percolation threshold with volume fraction $\phi = 0.15\%$.

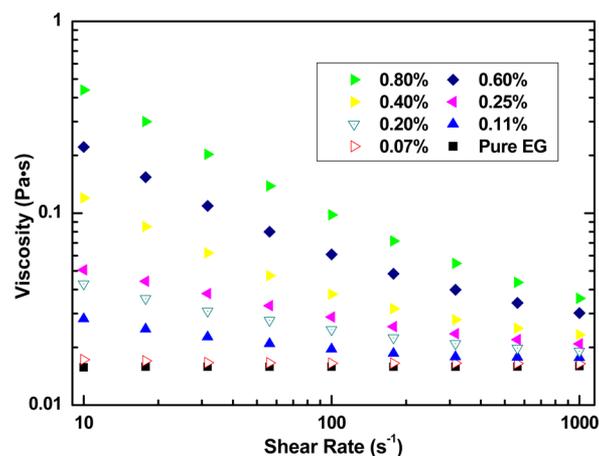


Figure 2. Viscosity of graphite–ethylene glycol suspensions with different volume fractions as a function of shear rate at room temperature. Non-Newtonian behavior (shear thinning) begins to dominate as the graphite volume fraction increases.

more rapidly with concentration below the percolation threshold than above percolation. To further study this effect we measured the thermal conductivity of the samples (following a similar preparation protocol as introduced in our previous paper¹⁷) used in the rheological characterization and

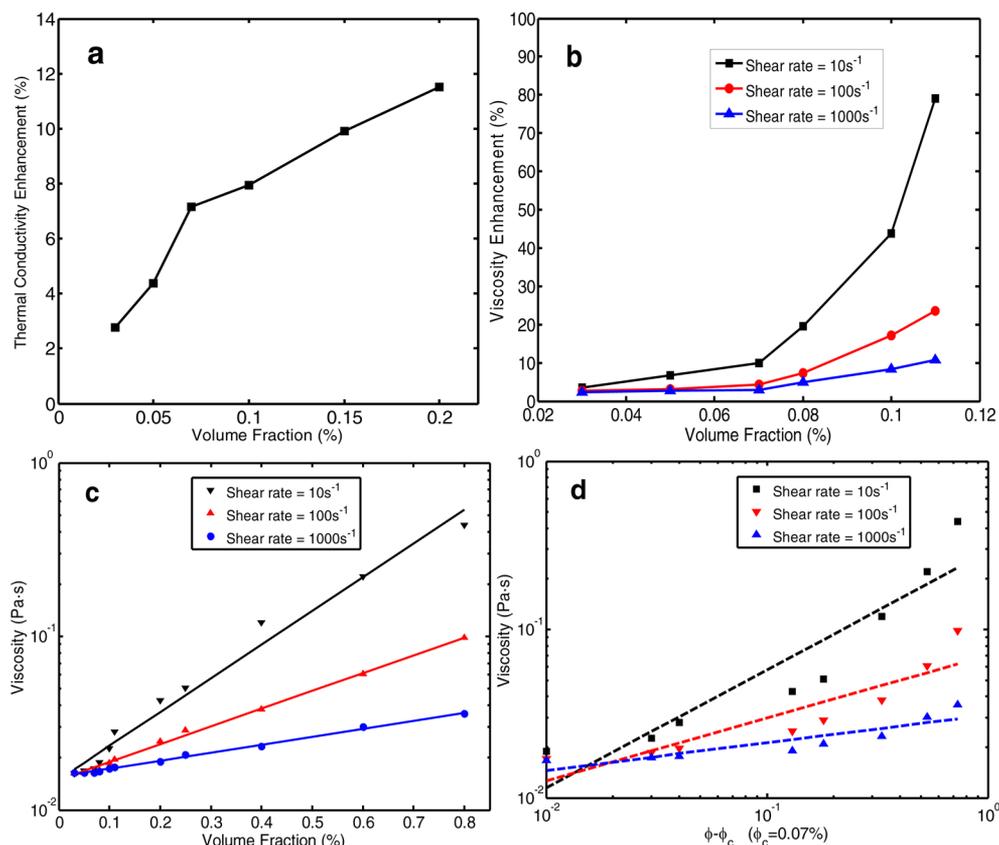


Figure 3. (a) Thermal conductivity enhancement of graphite suspensions as a function of volume fraction near the percolation regime. (b) Viscosity enhancement of graphite suspensions as a function of volume fraction near the percolation regime at given shear rates. (c) Viscosity as a function of volume fraction at different shear rates ($= 10, 100, \text{ and } 1000 \text{ s}^{-1}$). The solid lines are fitted using the Doolittle equation (the coefficients of determination $R^2 = 0.9930, 0.9989, \text{ and } 0.9962$ for shear rate $= 10, 100, \text{ and } 1000 \text{ s}^{-1}$, respectively). (d) Viscosity after percolation as a function of volume fraction at different shear rates ($= 10, 100, \text{ and } 1000 \text{ s}^{-1}$). The dash lines are fitted using power law (the coefficients of determination $R^2 = 0.6977, 0.7253, \text{ and } 0.7786$ for shear rate $= 10, 100, \text{ and } 1000 \text{ s}^{-1}$, respectively). The Doolittle equation fits much better than the power law.

the results are shown in Figure 3a. Note that below the percolation threshold (around 0.07 vol %), the thermal conductivity increases faster than above the percolation threshold, consistent with our previous report.^{17,46} Through prior AC impedance spectroscopy studies, we determined that this effect is due to tighter contact between individual graphite flakes below the percolation threshold, which arises as a result of energy minimization of isolated graphite clusters.¹⁷ In contrast to the thermal conductivity trend, the viscosity of the graphite suspensions increases much more rapidly after percolation than before percolation, as shown in Figure 3b. In addition, the viscosity dependence is well fitted with the Doolittle equation⁴⁷ $\eta(\phi) = A \exp(B(\phi/\phi_i)) = A \exp(B'\phi)$ (Figure 3c), rather than the weaker power law dependence (Figure 3d) observed for the electrical conductivity.^{17,46} Here A and B are numerical constants and ϕ_i is the free-space volume fraction of the suspension which is close to unity in our case because the particle volume fraction ϕ is less than 1%.

The effects of temperature on the thermal conductivity and viscosity of suspensions can provide further clues to the mechanisms behind the volume fraction dependence in addition to the importance of these properties for practical applications. The thermal conductivity of the suspension is measured by the transient hotwire method, which is a quite accurate and standard method for liquid thermal conductivity measurement with uncertainty about $\pm 1\%$. As shown in Figure 4, as the temperature varies from room temperature to 65 °C,

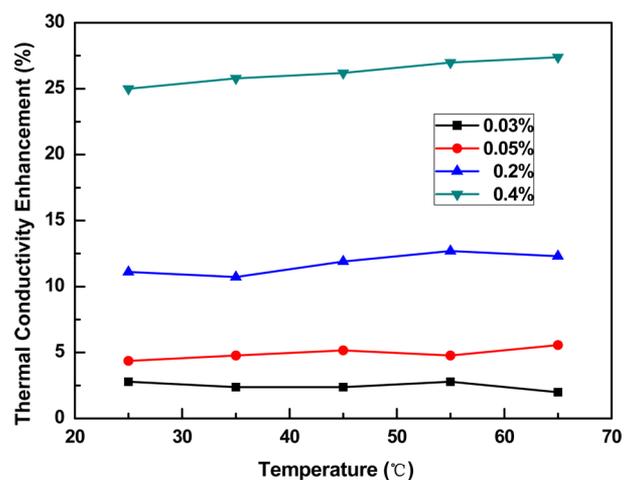


Figure 4. Thermal conductivity enhancement of graphite suspension as a function of temperature, showing that the enhancement is quite independent of temperature.

the enhancement in thermal conductivity does not vary significantly. This is consistent with the conclusion that Brownian motion of the dispersed particles is not responsible for the observed thermal conductivity enhancement in nanofluids.^{46,48–50}

The effect of temperature on the viscosity of nanofluids and suspensions, however, is more complex than its effect on the thermal conductivity. Figure 5a–c shows the steady shear

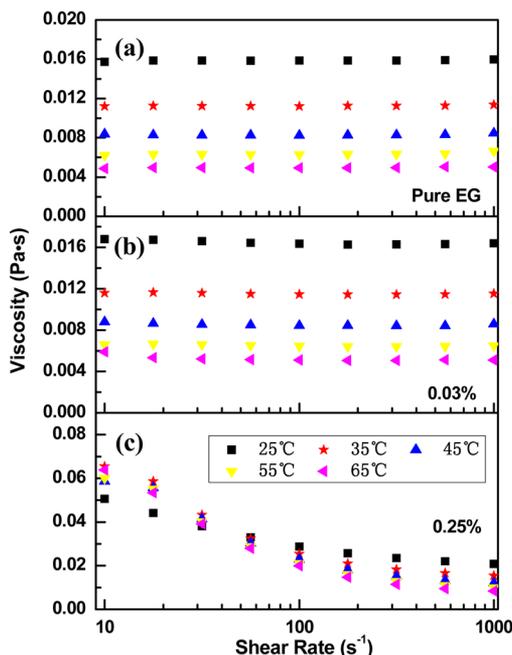


Figure 5. Steady shear viscosity of the graphite suspensions as a function of shear rate at different temperatures and different loadings. (a) Pure ethylene glycol (EG); (b) graphite–ethylene glycol suspension with 0.03 vol % graphite loading; (c) graphite–ethylene glycol suspension with 0.25 vol % graphite loading.

viscosity of several graphite suspensions as a function of shear rate at different temperatures and in Figure 6a–f we replot the data to clearly show the temperature dependence of viscosity at

different volume fractions and three selected values of the imposed shear rate. As the temperature increases from room temperature to 65 °C, the viscosity of the dilute suspensions, which show Newtonian behavior, is significantly reduced. Above the percolation threshold, the results are more complex (Figure 5c) and the variation with temperature is non-monotonic. We explore this complex thermorheological response in greater detail in Figure 6.

For dilute suspensions, the viscosity decreases with increasing temperature within the measured shear rate range (Figures 6a–c), similar to that of the pure solvent. At low shear rates, the viscosity depends strongly not only on temperature but also on the volume fraction (Figure 6a). However, at higher shear rates the variation in the viscosity between different volume loadings is reduced as the particles are increasingly shear-aligned (*cf.* Figure 6b,c). For concentrated suspensions, more interesting phenomena appear (Figure 6d–f). The viscosity is found to increase with increasing temperature (Figure 6d) at low shear rates but then change to the reverse behavior at high shear rates (Figure 6f).

To understand the thermorheological behavior of these nanofluids, we first consider the temperature-dependence of the suspending solvent. The pure solvent viscosity $\mu_s(T)$ can be described by a thermally rate-activated process of Arrhenius type so that $\mu_s(T) = \mu_0 \exp[(\Delta H/R)(1/T - 1/T_0)]$,⁵¹ where R is the ideal gas constant, ΔH is the energy barrier for the solvent molecules to make a transition from an original energy state to a new energy state under imposed shearing, and μ_0 is the viscosity of the solvent at the reference temperature T_0 . This leads to a decrease in the viscosity of the solvent with increasing temperature.^{52–54} Regression to the pure ethylene glycol data in Figure 6a gives $\Delta H/(RT_0) = 9.977$, $\mu_0 = 0.0147$ Pa·s at $T_0 = 300$ K.

The rheology of concentrated suspensions has been studied extensively.^{55–59} Brady and co-workers^{60–64} have developed a Stokesian dynamics approach that is widely used to predict the

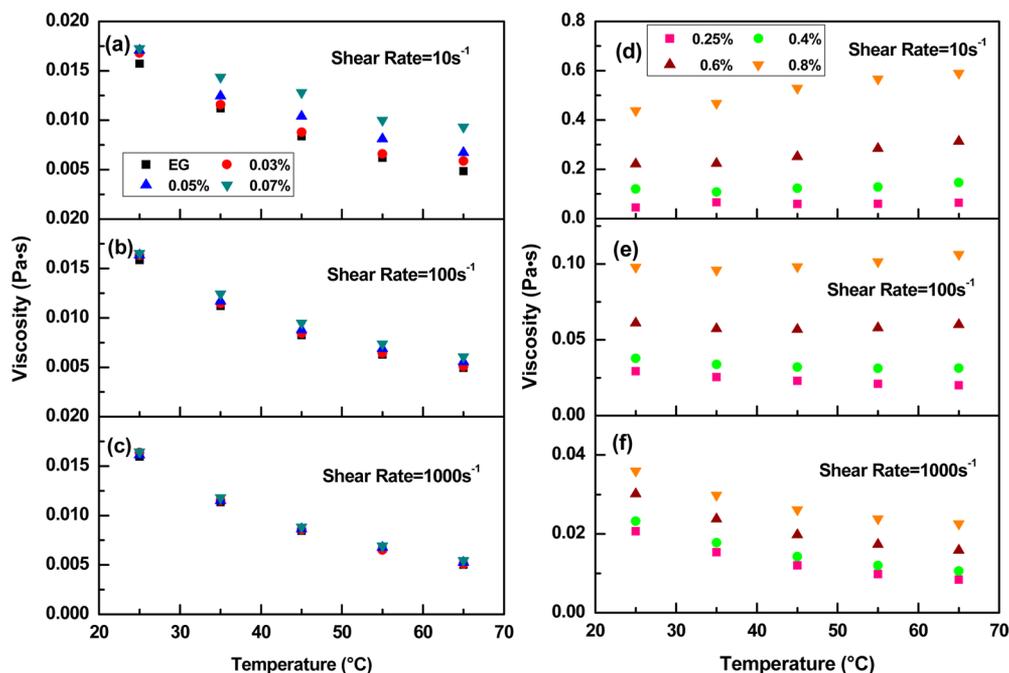


Figure 6. Viscosity as a function of temperature at different graphite volume fractions; (a–c) below percolation threshold, and (d–f) above percolation threshold. The temperature dependence of the viscosity changes above the percolation threshold from low shear rates to high shear rates.

microstructural properties and macroscopic properties of hard-sphere suspensions. Although the dispersed graphite flakes are not hard spheres, we found that our experimental data can be rationalized using ideas from Stokesian dynamics simulations when combined with understandings of the structures of the graphite flakes in the suspensions, in particular, the observation that the graphite flakes are closely aggregated into isolated clusters below the percolation threshold due to global surface energy minimization while above the percolation threshold, the contact between flakes weakens, as supported by our previous AC impedance studies.^{17,46}

The relevant dimensionless parameter when discussing relative contributions to the viscosity of a Brownian dispersion or suspension viscosity is the Péclet number $Pe = \tau_D/\tau_S$ that relates the characteristic diffusive time scale τ_D of the dispersed phase to the characteristic flow time scale τ_S . A large Péclet number means that the applied shearing deformation dominates while a small Péclet number means Brownian motion is dominant. The characteristic convective time scale at a given imposed shear rate $\dot{\gamma}$ is $\tau_S = 1/\dot{\gamma}$. The characteristic time scale for diffusion is $\tau_D \sim a^2/D$, where a is the Stokes radius of the particle, and D is the translational diffusion coefficient. The diffusion coefficient can be calculated from the well-known Einstein relation $D = (k_B T)/f$, where f is the friction coefficient, and this relation is valid for arbitrary shape particles. For spherical particle with radius a , $f = 6\pi\mu(T)a$ and $\tau_D = (6\pi\mu(T)a^3)/(k_B T)$. Thus, the Péclet number for spherical particles is $Pe = (6\pi\mu(T)\dot{\gamma}a^3)/(k_B T)$. As the temperature increases, the characteristic time scale for Brownian motion reduces since $\mu(T)/T$ decreases and the Péclet number decreases. For nonspherical particles, the more relevant dimensionless parameter is a rotational Péclet number in which τ_D is the characteristic time scale of particle reorientation caused by Brownian motion. If we approximate the shape of graphite flakes as circular disks with diameter $2a$, then $\tau_D = (32\mu(T)a^3)/(3k_B T)$ and the Péclet number becomes $Pe = (32\mu(T)\dot{\gamma}a^3)/(3k_B T)$.⁶⁵ Note that both the translational and rotational Péclet numbers have similar functional forms and are proportional to $(\mu(T)\dot{\gamma}a^3)/(k_B T)$ (where a^3 is proportional to the particle hydrodynamic volume), and the difference lies only in the numerical prefactor. Because our graphite flakes are neither spherical particles nor perfect circular disks, we neglect the specific value of the numerical prefactor when calculating the Péclet number for our system as it simply shifts the magnitude of Péclet number by a constant factor. For dilute suspensions, as inferred from prior works on the same system, the graphite flakes are quite tightly aggregated into isolated clusters.¹⁷ In this dilute regime we should consider these isolated clusters, not individual graphite flakes, as the relevant Brownian objects. Note that the typical size of a graphite cluster observed via optical microscopy is on the order of $\sim 100 \mu\text{m}$, which is 2 orders of magnitude larger than the lateral size of an individual graphite flake so that the hydrodynamic volume of the cluster is about 6 orders of magnitude larger than the flake volume. The large graphite cluster size, which gives a relatively large Péclet number, indicates the insignificance of Brownian motion on the motion of the clusters even at low imposed shear rates. As the shear rate is increased, the contribution of Brownian motion to the total viscosity of the clustered dispersion becomes increasingly negligible, as indicated by the smaller and smaller difference between different volume loadings (Figure 6b,c).

For more concentrated suspensions, the graphite clusters merge together and form a sample-spanning percolation

structure. The driving force to minimize the surface energy of isolated clusters becomes smaller thus the contact between graphite flakes becomes looser, as supported by our AC impedance spectroscopy studies reported in a previous study.¹⁷ This reduced contact allows individual graphite flakes increasing freedom to diffuse. Brownian motion of individual graphite flakes thus becomes more important in the percolated regime, especially when the imposed shear rate $\dot{\gamma}$ is sufficiently low.

To quantitatively understand the inverted trends of the viscosity observed in Figure 6d,f for samples above the percolation threshold, we plot the viscosity of concentrated suspensions as a function of the Péclet number for several characteristic shear rates in Figure 7. To calculate the Péclet number, we estimate the average flake lateral size $2a$ observed in SEM to be on the order of $\sim 1 \mu\text{m}$ so that $a^3 \sim 10^{-18} \text{ m}^3$. In our experiments, the Péclet number can be varied by changing not only the shear rate $\dot{\gamma}$ but also temperature via the Arrhenius thermal dependence of $\mu(T)$ for the ethylene glycol solvent. In Figure 7, the Péclet number variation is due to the temperature change since the shear rate is held fixed in each subfigure. When the shear rate is small (10 s^{-1}), the flow is in the low Péclet number regime (Figure 7a) and diffusive contributions dominate the suspension viscosity. As a consequence, even though the temperature rise causes a decrease of the solvent viscosity the measured suspension viscosity still increases with the increasing temperature. However, when the shear rate is high (1000 s^{-1}), the Péclet number is orders of magnitude higher and the total dissipation in the system is now dominated by locally advective hydrodynamic effects (Figure 7c). The Brownian motion of graphite flakes becomes much less important and hence the suspension viscosity closely follows the solvent viscosity trend as the temperature is increased.

The transition from Brownian-motion dominated diffusive behavior to shear-dominated convective behavior is well summarized in Figure 8, which plots the viscosity versus Péclet number for the 0.8% volume fraction dispersion at different shear rates in a single chart. In Stokesian dynamics studies of the shear thinning to shear thickening transition beyond a critical Péclet number, the transition Péclet number was achieved mainly by changing the shear rate.⁶⁶ The critical Péclet number for the shear thinning to shear thickening transition is usually around $Pe_{\text{crit}} \sim 10\text{--}100$ or even higher, depending on the interaction among particles.⁶⁷ By tuning both the shear rate and the temperature dependence of the base fluid viscosity, we can also clearly observe a similar transition for the suspension viscosity which first decreases with Péclet number and then increases with Péclet number (Figure 8). Finally, we note that if we define a relative viscosity $\eta_r = \eta(T,\dot{\gamma})/\mu_s(T)$ using the temperature-dependent base fluid viscosity, all of the data points shown in Figure 8 at a given volume fraction collapse to a single master curve (which is shown in the inset of Figure 8).

In summary, we have observed markedly different trends in the concentration-dependence of the shear viscosity and thermal conductivity of graphite suspensions below and above the percolation threshold. Below the percolation threshold, the thermal conductivity increases with volume fraction more rapidly with concentration than above the threshold, while the viscosity behaves in the inverse fashion. The increase in the thermal conductivity is found to be almost independent of temperature; however, the shear viscosity shows a complicated thermorheological behavior. Below the percola-

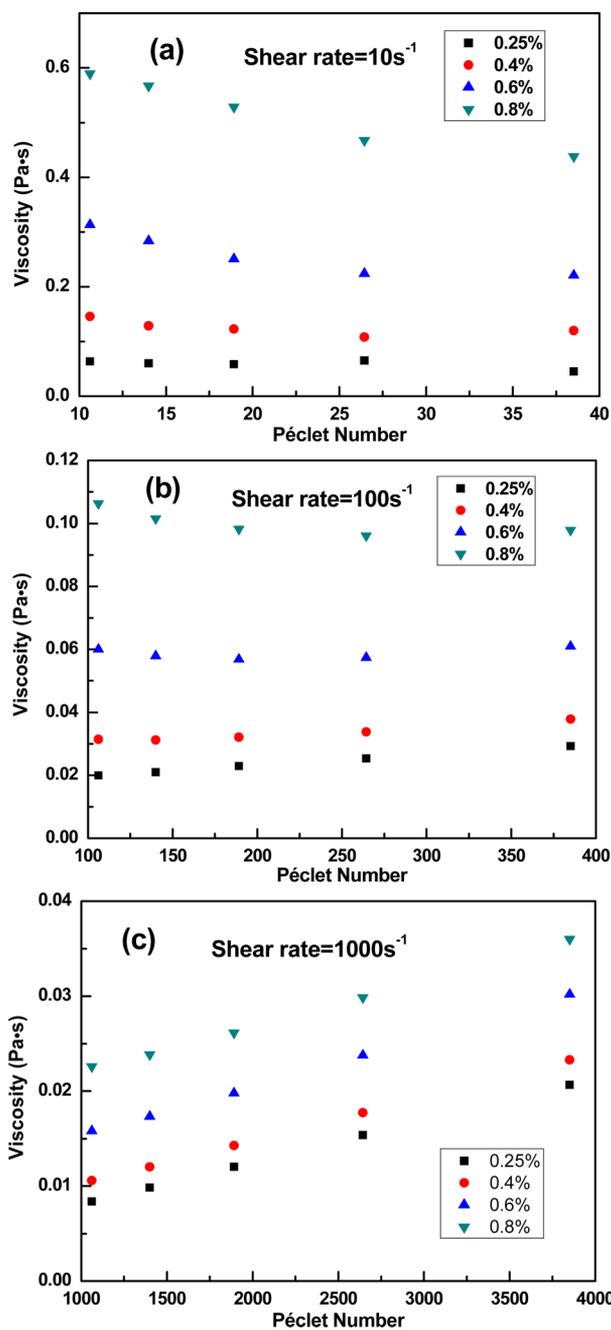


Figure 7. Viscosity of several suspensions at specified shear rates plotted as a function of the dimensionless Péclet number which is varied by increasing the temperature from 25 to 65 °C.

tion threshold, the viscosity decreases with increasing temperature at all shear rates studied, while above the percolation threshold the viscosity of the percolated network initially increases with increasing temperature at low shear rates but this switches to a decreasing trend at high shear rates. The complicated thermal dependence of the shear viscosity can be understood by considering the Péclet number of the dispersion in conjunction with the evolution in the microstructure of the suspensions below and above the percolation threshold, which has been established through previous AC impedance spectroscopy studies. Below percolation, the graphite flakes form closely aggregated, isolated clusters. The diffusive Brownian contribution of these large clusters to the total viscosity is

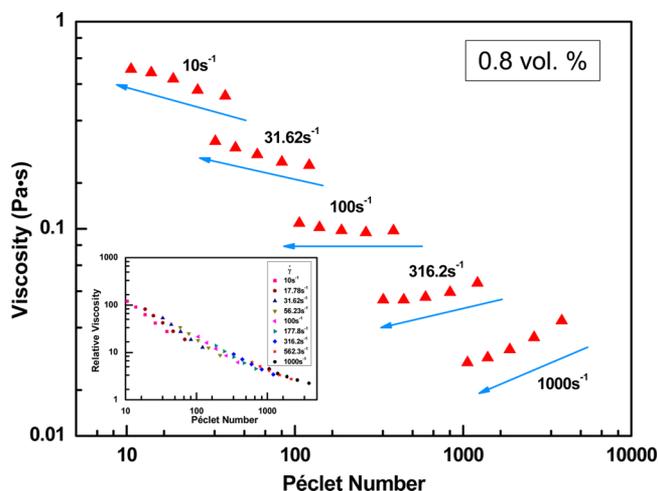


Figure 8. Viscosity as a function of Péclet number for 0.8 vol % dispersion of graphite flakes at several characteristic shear rates. The arrow indicates the direction of temperature increases from 25 to 65 °C. The inset shows that all the data points collapse to a single master curve when nondimensionalizing the viscosity by the temperature dependent viscosity of the base fluid to give a relative viscosity $\eta_r = \eta(\dot{\gamma}, T) / \mu_s(T)$.

negligible. Above the percolation threshold, the surface energy of the isolated clusters is reduced and the diffusive motion of individual graphite flakes plus attractive interactions between the flakes become important. At low imposed shear rates, these interactions between the individual flakes and Brownian motion dominate and thus the viscosity increases with temperature. At high shear rates, the percolated network is disrupted, the particles are aligned by the flow and locally advective hydrodynamic contributions to the total dissipation in the dispersion dominate the measured shear stress, leading to shear-thinning. The insights gained from this thermorheological study will help better understanding of structure–property relations of nanostructured dispersions. From an application viewpoint, our studies of both the viscosity and thermal conductivity enhancements with nanoparticulate loading suggest that potential application of nanofluids in convective heat transfer should be focused on fluids below the percolation threshold as the shear viscosity (and thus the viscous energy dissipation) of the nanofluids and suspensions increases exponentially after crossing the percolation threshold, whereas the incremental gains from enhanced heat transfer are minimal.

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Notes

The authors declare no competing financial interest.

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